



**ASSESSMENT OF A 1 Psi REDUCTION IN THE RVP OF
CONVENTIONAL GASOLINE BLENDSTOCK (CBOB)
IN THE SUMMER GASOLINE SEASON**

Prepared for

THE RENEWABLE FUELS ASSOCIATION

By

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INTRODUCTION AND EXECUTIVE SUMMARY

The Renewable Fuels Association (RFA) retained MathPro Inc. to conduct a first-order analysis to estimate the additional costs that would be incurred by U.S. refiners if the RVP of conventional gasoline blendstock (CBOB) were reduced by 1 psi for the summer season – from about 9 psi to 8 psi. The proposed 1 psi reduction in RVP would apply to most CBOB produced for sale in the U.S.¹

This report is the primary work product of this study.

Background

On July 2, 2021, the U.S. Court of Appeals for the D.C. Circuit overturned the rule (the “E15 rule”) issued by EPA on June 10, 2019, extending to E15 gasoline the 1 psi ethanol RVP waiver for conventional gasoline in the summer ozone control season (June 1–September 15). Previously, the RVP waiver had applied only to E10 gasoline. The E15 rule allowed retailers in conventional gasoline (CG) markets to sell both finished E10 and E15 with RVP of 10 psi during the summer season. The E15 rule was designed to facilitate year-round supply of E15 gasoline, by allowing use of the same 9 RVP CBOB in blending either E10 or E15 finished CG in the summer. With the E15 rule overturned, retailers will again have to ensure that any E15 they sell in the summer season meets the prevailing 9 RVP standard for finished CG, while E10 continues to qualify for a 1 psi allowance via the ethanol RVP waiver. The Court’s ruling leaves E15 economically uncompetitive with E10 in conventional gasoline markets in the summer season, thereby foreclosing an important pathway for increasing ethanol’s share of the gasoline market.

In response, RFA is considering requesting that EPA, using its authority under the Clean Air Act, establish an RVP standard for CBOB of 8 psi. This would require refiners to reduce the current RVP of CBOBs by about 1 psi during the summer season -- from about 9 RVP to 8 RVP. When blended with an 8 RVP CBOB, E15 and E10 gasolines both would meet the 9 RVP standard for finished summer CG, making the use of the RVP waiver for E10 unnecessary. This would allow E15 to be produced using E10 CBOBs and restore the blending options for E15 prevailing before the Court’s decision disallowing the use of the ethanol RVP waiver for E15, albeit with both finished E10 and E15 gasolines having lower RVPs.

Implementing the proposed reduction in the RVP of CBOB would increase the refining sector’s cost of RVP control. Consideration of such costs would be a key element in any rule-making that EPA would undertake.

¹ Conventional gasoline not qualifying for the ethanol RVP waiver (upstate New York), low-RVP gasoline, and RFG would not be affected.

Technical Approach

Our analysis covers U.S. regional refining operations in the *summer* gasoline season in each of four refining regions: PADD 1, PADD 2, PADD 3, and PADD 4.²

We conducted the analysis by means of regional refinery LP modeling, using MathPro's proprietary refinery modeling system, **ARMS**. We applied four models, each one representing aggregate refining operations in one of the PADDs. We developed the four regional refining models by updating corresponding regional refining models developed in a recent study for EPA.³

The target time period for the analysis here was the 2019 summer gasoline season.⁴

Starting from the EPA study and using primarily EIA data sources, we developed regional (i.e., PADD-level) representations of (1) regional refinery production of gasoline – CG, low-RVP CG, and federal RFG – and other refined products, (2) aggregate refinery process capacities, (3) regional aggregate crude oil slates, and (4) composite crude oil costs, all for 2019.

The refinery modeling for *each region* encompasses a Baseline (Reference) Case, and a 2019 Study Case, all for the summer gasoline season.

- The regional *Baseline* cases represent regional refining operations in the 2019 summer season producing, among other refined products, summer finished E10 CG with 10 RVP (i.e., meeting the 9 RVP standard adjusted for the 1 psi ethanol waiver), as well as meeting all other prevailing gasoline standards, including octane ratings, sulfur content (10 ppm average) and benzene content (0.62 vol% average).
- The regional *Study* cases likewise represent the same regional refining operations in the 2019 summer season, but producing summer finished E10 CG with 9 RVP. This requires CBOBs meeting an 8 psi RVP standard – a 1 psi reduction from the current RVP of CBOBs. Otherwise, the Study cases are identical to the Baseline cases.

For each region, the differences between the solutions returned by the refining models for the Baseline and Study Cases indicated the estimated refining costs of reducing the RVP of CBOBs by 1 psi, as well as the changes in refining operations accounting for those costs.

The analysis also included a set of regional *Sensitivity* Cases, to assess the sensitivity of the estimated refining costs to a significant change in average crude oil cost. Each Sensitivity Case

² We did not consider PADD 5 in the analysis, because most ($\approx 75\%$) of the gasoline in PADD 5 is reformulated gasoline produced in California, meets stringent RVP standards, and does not qualify for the ethanol RVP waiver.

³ EPA Contract No. EP-C-16-020; Work Assignment Nos. 0-11 and 1-11; July 2018

⁴ We used 2019 as the target year because the required data for that year was readily available; it is the most recent pre-pandemic year; and gasoline demand in 2019 is representative of demand in the next several years, as projected by EIA and others.

differed from the corresponding Study case only in the assumed composite crude oil costs (\approx \$100/b in the Sensitivity cases vs. \approx \$60 in the Study cases).

Results of the Analysis

Study Cases

Table ES-1 summarizes the primary results of the Study Cases. It shows, for each of the four regions considered and for the U.S. (ex PADD 5), the estimated costs in the refining sector – capital investment, annual refining cost, and per-gallon refining cost – of producing summer CBOB meeting a new 8 psi RVP standard⁵ – a 1 psi reduction from current CBOB RVP.

Table ES-1: Primary Results of the Study Cases

| | Region | | | | Total |
|--|--------|--------|--------|--------|-------|
| | PADD 1 | PADD 2 | PADD 3 | PADD 4 | |
| Composite Crude Oil Cost (\$/b) | 66 | 57 | 62 | 54 | 61 |
| Finished Gasoline Volume ¹ (K b/d) | 66 | 1,546 | 2,351 | 270 | 4,233 |
| Capital Investment (\$MM) | 17 | 147 | 88 | 30 | 282 |
| Summer Refining Cost (\$MM) | 18 | 258 | 374 | 44 | 694 |
| Refining Operations | 14 | 214 | 347 | 35 | 610 |
| Capital Charge & Fixed Costs | 5 | 44 | 27 | 9 | 84 |
| Per-Gallon Refining Costs ² (ϕ /gal) | 3.6 | 2.2 | 2.1 | 2.1 | 2.1 |
| Refining Operations | 2.7 | 1.8 | 1.9 | 1.7 | 1.9 |
| Capital Charge & Fixed Costs | 0.9 | 0.4 | 0.1 | 0.4 | 0.3 |
| Energy Density-Related Savings ² (ϕ /gal) | 0.8 | 0.7 | 0.7 | 0.5 | 0.7 |
| Net Cost ³ (ϕ /gal) | 2.9 | 1.5 | 1.4 | 1.6 | 1.5 |

1 Summer E10 CG qualifying for the ethanol RVP waiver.

2 Per gallon of Summer E10 CG qualifying for the RVP waiver.

3 Per-Gallon Refining Costs less Energy Density-Related Savings.

The estimated per-gallon costs of the additional RVP control are higher in PADD 1 than in PADDs 2, 3, and 4. The reason for this is discussed in the report.

As **Table ES-1** shows, the estimated U.S. total capital investment and annual refining cost of the 1 psi reduction in RVP are about **\$280 million** and **\$700 million/year**, respectively. The estimated average gross national per-gallon cost of achieving the 1 psi RVP reduction is about **2.1 ϕ /gal** for the affected gasoline pool – summer E10 CG qualifying for the ethanol RVP waiver. (In practice, the aggregate investments and capital charges may be lower than indicated because some refineries may have already adequate throughput capacity to handle additional RVP control.)

Table ES-1 also shows the estimated energy density-related savings resulting from the proposed reduction in the RVP standard. For reasons explained in the report (Section 1), reducing gasoline

⁵ We assumed that refiners would produce CBOBs with RVP \leq 7.7 psi at the refinery gate, 1 psi lower than current CBOB RVP of about 8.7 psi.

RVP (all else equal) would lead to a small increase in the energy density (BTU/gal) of the gasoline pool and a resulting slight increase in average fuel economy (miles/gal). The increase in average fuel economy would serve to decrease the *national (or social) cost* of gasoline consumption, partially offsetting the *refining cost* of an 8 RVP CBOB standard. The increase in fuel economy would be an economic benefit to consumers, not the refining sector.

Accordingly, the estimated *national (net)* per gallon cost of an 8 RVP standard is about **1.5¢/gal**.

Sensitivity Cases

Table ES-2 summarizes the primary results of the Study Cases and the Sensitivity Cases. These results indicate, for each of the four regions considered and for the U.S. (ex PADD 5), the relatively small degree to which a significant change in composite crude oil costs would affect the estimated costs in the refining sector – capital investment, annual refining cost, and per-gallon refining cost – of producing summer CBOB meeting an 8 psi RVP standard.

Table ES-2: Primary Results of the Study Cases and Sensitivity Cases

| | Region | | | | Total |
|---|--------|--------|--------|--------|-------|
| | PADD 1 | PADD 2 | PADD 3 | PADD 4 | |
| Composite Crude Oil Cost (\$/b) | | | | | |
| Study Case | 66 | 57 | 62 | 54 | 61 |
| Sensitivity Case | 107 | 94 | 101 | 89 | 100 |
| Finished Gasoline Volume¹ (K b/d) | | | | | |
| Study Case | 66 | 1,546 | 2,351 | 270 | 4,233 |
| Sensitivity Case | 66 | 1,546 | 2,351 | 270 | 4,233 |
| Capital Investment (\$MM) | | | | | |
| Study Case | 17 | 147 | 88 | 30 | 282 |
| Sensitivity Case | 32 | 165 | 121 | 33 | 351 |
| Summer Refining Cost (\$MM) | | | | | |
| Study Case | 18 | 258 | 374 | 44 | 694 |
| Refining Operations | 14 | 214 | 347 | 35 | 610 |
| Capital Charge & Fixed Costs | 5 | 44 | 27 | 9 | 84 |
| Sensitivity Case | 21 | 309 | 443 | 47 | 820 |
| Refining Operations | 12 | 261 | 406 | 36 | 714 |
| Capital Charge & Fixed Costs | 9 | 50 | 39 | 11 | 109 |
| Per-Gallon Refining Costs² (¢/gal) | | | | | |
| Study Case | 3.6 | 2.2 | 2.1 | 2.1 | 2.1 |
| Refining Operations | 2.7 | 1.8 | 1.9 | 1.7 | 1.9 |
| Capital Charge & Fixed Costs | 0.9 | 0.4 | 0.1 | 0.4 | 0.3 |
| Sensitivity Case | 4.2 | 2.6 | 2.5 | 2.3 | 2.5 |
| Refining Operations | 2.4 | 2.2 | 2.2 | 1.7 | 2.2 |
| Capital Charge & Fixed Costs | 1.8 | 0.4 | 0.2 | 0.5 | 0.3 |
| Energy Density-Related Savings² (¢/gal) | | | | | |
| Study Case | 0.8 | 0.7 | 0.7 | 0.5 | 0.7 |
| Sensitivity Case | 0.3 | 1.0 | 1.0 | 0.9 | 1.0 |

1 Summer E10 CG qualifying for the ethanol RVP waiver.

2 Per gallon of Summer E10 CG qualifying for the RVP waiver.

Table ES-2 indicates that even a substantial change in crude oil prices would have only moderate effect on the capital and operating costs that the refining sector would incur in reducing the RVP of summer CBOB to meet an 8 RVP standard.

Contents of the Report

Section 1 of the report identifies the technical factors involved in controlling the RVP of refinery-produced gasoline. Section 2 summarizes the analytical approach and methodology for the analysis. Section 3 presents the key results of the analysis and discusses these results.

Appendix A provides additional detail on the analytical methodology used in this study.

Appendix B provides additional detail (in tabular format) on the input data and the results of the analysis.

1. TECHNICAL FACTORS INVOLVED IN RVP CONTROL

Refiners could reduce summer gasoline RVP from current levels to the levels considered in this analysis by several routes, either alone or in combination (depending on the RVP standard, refinery crude slate, and refinery configuration). In most situations, the most economical route to reducing the RVP of all or part of a refinery's gasoline pool would be to reduce the concentration of butanes (C4 material) in the gasoline. The butanes are constituents of crude oil and natural gas liquids, and they are produced in certain refining process. They are the lightest and most volatile – highest RVP – constituents of gasoline. Though their volume in the gasoline pool is small, their high RVP has a disproportionate effect on the RVP of the gasoline pool. But they have high octane.

1.1 Removal of Volatile Components – Debutanization

The most economical and direct way to remove butanes from the gasoline pool is by means of a standard distillation process, called *debutanization*. All gasoline-producing refineries have debutanizers, processing various refinery streams (primarily light FCC naphtha and straight run naphtha, but also alkylate, isomerate, and light hydrocracked naphtha). Reducing CBOB RVP to meet an 8 psi standard (corresponding to about 7.7 psi before ethanol blending) should be feasible in many refineries through enhanced debutanization alone. If further RVP control were required, debutanization can be supplemented with depentanization (C5 removal) of certain refinery streams.

Because of the tight specification on the pentanes content of butane sold as LPG or petrochemical feedstock, the debutanization must be performed so as to leave some C4s in the C5+ material going to the gasoline pool. However, suitably upgrading refinery debutanization facilities and light ends recovery systems to sharpen the C4/C5 separation can reduce the butane content of the gasoline pool to ≤ 1 vol%, without degrading the quality of sales butane. This approach involves (1) modifying debutanizers to take more pentanes (C5s) overhead (i.e., commingled with the butanes) at the processing units where they are produced, thereby reducing the butane content of the debutanized streams, and (2) sending the debutanizer overhead streams (containing mostly C4s but with some C5s) to a refinery light ends plant designed to make a sharp C4/C5 separation. The essentially butane-free C5 material leaving the light ends unit can be blended to gasoline or segregated for other dispositions.

1.2 Replacement of Lost Octane and Volume

The butanes have high octane (92-94 AKI), higher than the average octane of the U.S. gasoline pool. Indeed, their octane is sufficiently high so that some refiners buy butanes in the winter season, when the RVP standard is much less stringent than in the summer, to blend into their winter gasoline pool as an economical source of incremental octane.

Consequently, when refiners remove butanes from the gasoline pool for RVP control, they must replace not only the lost volume but also the lost octane, in order to maintain constant volume and octane in their gasoline pool. Doing so involves some combination, unique to each refinery, of:

- Increasing reformer severity and throughput, for octane and volume replacement
- Small increases in utilization of alkylation capacity, for octane and volume replacement
- Small increases in capacity utilization for various processes
- Additional crude oil throughput, to provide additional feedstock for reforming and other operations

Reducing gasoline RVP may require further changes in refinery operations. For example, it may require rejecting some heavy gasoline components to the distillate fuel pool, to maintain compliance with other gasoline standards.

The gasoline blendstocks that would be added to the gasoline pool to replace the butane (and possibly) pentane removed for RVP control are all heavier and denser (in lb/gal) the butane and pentane they replace. This would lead to a small increase in the average fuel economy of the gasoline pool.

Refinery LP modeling, such as that conducted in this study, is the method of choice for capturing the various interactions between processing options and selecting the least cost route for achieving the desired objective – in this case, more stringent RVP control for summer CBOB.

1.3 Disposition of Butanes Removed from Summer Gasoline

The dispositions of C4s (and possibly C5s) removed from the summer gasoline pool are outside the realm of seasonal refinery modeling. But these dispositions influence the economics of RVP control, and we therefore addressed them in the analysis. The alternative dispositions of these streams include:

- Storing them, either at the refinery or a remote storage facility, for use in the winter season (or, equivalently, selling them to a third party in the summer and purchasing them in the winter);
- Using them as alkylation feed, with investment, if needed, to expand and/or revamp alkylation capacity;
- Using them as hydrogen plant feed, to displace purchased natural gas;
- Selling the C4s into the LPG market; and
- Using them as refinery fuel or selling them at a distressed price level approximating fuel value.

The first option, inter-seasonal transfer, implies that the butanes and pentanes (if any) removed and stored in the summer season become refinery inputs, in like volumes, in the winter season. Refineries would have an economic incentive to practice inter-seasonal transfer if the marginal values of the butane and pentane in the winter are greater than the sum of (1) the cost of inter-seasonal transfer and (2) their value in the summer in alternative uses (e.g., as refinery fuel) or as an LPG component.

The marginal values of butane and pentane tend to be higher in the winter than in summer because of the relaxed RVP standards in the winter. Butane and pentane can be used in the winter to maintain gasoline and other refined product out-turns with reduced crude through-put and other cost-reducing changes in refinery operations.

Each refinery would face its own set of circumstances – geographic and economic – that would influence its disposition of choice for butane (and possibly pentane) removed from the summer gasoline pool.

For this study, we simply assumed that the relatively small additional volumes of produced-butane would be sold at prices prevailing during the summer season of 2019.

2. REFINERY MODELING METHODOLOGY

We analyzed the refining economics of the proposed RVP standard by means of four refinery LP models, representing regional refining operations in PADD 1, PADD 2, PADD 3, and PADD 4, respectively.

We did not consider PADD 5 in the analysis, because (i) most ($\approx 75\%$) of the gasoline volume produced and consumed in PADD 5 is produced in California, the RVP standard for California gasoline is already more stringent than 8 psi (and the ethanol RVP waiver does not apply).

We developed the four refining models used in this study from regional refining models calibrated to summer 2016 from a recent study conducted for EPA (referenced earlier). The regional models are distinct in terms of aggregate refining process capacity, composite crude oil slate, refinery inputs and outputs, refined product specifications, and other region-specific elements. The target time period for this analysis is the 2019 summer gasoline season.

2.1 Cases Analyzed with the Refining Models

2.1.1 Calibration/Baseline Cases (2019)

We updated regional refining models from the EPA study so that they reflected refining operations in summer 2019. Specifically, we:

- Incorporated the Tier 3 gasoline sulfur standard (average sulfur level in gasoline < 10 ppm);
- Modified refinery inputs and outputs to reflect data reported by EIA for summer 2019;
- Modified refining process capacity to reflect EIA's refinery-by-refinery process capacity reported as of January 2019;
- Updated crude oil acquisition costs, energy prices, and LPG prices as reported by EIA;
- Updated representations of composite crude oils to reflect reported API gravities and sulfur content, relative shares of domestic and imported crude oils, and properties of refinery imports of crude oil;
- Adjusted certain model coefficients so as to more closely represent butane balances in summer 2019;
- Adjusted capacities for minor process representations not reported by EIA, but that are required processes for refinery modeling (e.g., debutanization, naphtha splitting), as needed; and
- Maintained the environmental fuel standards represented in the 2016 models, such as MSAT 2 and ULSD standards.

Solutions returned by the regional refining models for these cases constitute the baseline values for the analysis.

2.1.2 Study Cases (2019)

The Study Cases differ from the corresponding Baseline Cases only in the RVP standard for CBOB.

Comparison of the results returned by each regional refining model for its Study Case with the results returned for the corresponding Baseline Case yielded estimates of the investment requirements and refining costs associated with the contemplated RVP standard.

2.1.3 Sensitivity Cases (2019)

Crude oil acquisition is by far the largest cost that refiners incur. For that reason, we chose it as the one input assumption to vary in a sensitivity analysis. The crude oil prices in the regional Study Cases are average regional refinery acquisition costs reported by the EIA for 2019.

The (significantly higher) crude oil acquisition costs in the Sensitivity Cases reflect an assumed U.S. average crude oil acquisition cost of \$100/b. This is comparable to average refinery acquisition costs (in nominal terms) in 2010-2014 – that is, to crude oil prices that the U.S. has experienced at times in the last decade. We considered these prices as representative of crude oil acquisition costs that *could* be experienced again in, say, the next decade. Crude oil acquisition costs for each PADD, relative to the assumed national \$100/b average, were estimated based on patterns of crude oil acquisition costs reported over the last decade

The *Sensitivity* Cases in the analysis serve to assess the sensitivity of the estimated refining costs to a significant change in average crude oil acquisition costs. The Sensitivity Cases differ from the corresponding Study Cases only in the average crude oil acquisition costs (and in the prices of propane and butanes, which were increased in step with the increased crude oil prices).

Table 2.1 shows the regional average crude oil acquisition costs in the Study Case and in the Sensitivity Case, for the 2019 summer season.

**Table 2.1: Average Cost of the Composite Crude Oil in the Refining Models
2019 Summer Season, (\$/b)**

| | Region | | | | U.S |
|-------------------------|------------|-----------|------------|-----------|------------|
| | PADD 1 | PADD 2 | PADD 3 | PADD 4 | |
| Study Case | 66 | 57 | 62 | 54 | 61 |
| Sensitivity Case | 107 | 94 | 101 | 89 | 100 |

2.2 Key Elements of the Methodology

- The Baseline, Study, and Sensitivity Cases represent virtually all finished gasoline (for domestic consumption) as ethanol-blended at 10 vol% (E10) (with only minimal production of E85).
- The Baseline, Study, and Sensitivity Cases incorporate regional refinery crude slates comparable to those in 2019.
- The Study and Sensitivity Cases represent the U.S. refining sector maintaining regional gasoline production at the 2019 Baseline volumes.

Table 2.2 shows the estimated regional distribution (in terms of volumes and volume shares) of the various gasoline types produced in U.S. refineries, by region. These values apply in the models for the Baseline, Study, and Sensitivity Cases. They were derived from various EIA and EPA data sources.

The **Total** volumes and the corresponding volume shares (**Share**) in Table 2.2 do not include PADD 5 volumes or imports (which are mainly to PADD 1).

Table 2.2: Distribution of Gasoline Production by Gasoline Type and PADD, Summer 2019

| Gasoline Type | Region | | | | Total |
|-----------------------|-------------|--------------|--------------|-------------|--------------|
| | PADD 1 | PADD 2 | PADD 3 | PADD 4 | |
| Volume (K b/d) | 532 | 2,198 | 4,642 | 356 | 7,728 |
| RFG | 332 | 278 | 830 | 0 | 1,440 |
| Conventional, waiver | 66 | 1,546 | 2,351 | 270 | 4,233 |
| Low-RVP | 112 | 340 | 713 | 83 | 1,248 |
| Clear (no Eoh) | 5 | 21 | 32 | 3 | 61 |
| Export | 17 | 13 | 716 | 0 | 746 |
| Share (%) | 100% | 100% | 100% | 100% | 100% |
| RFG | 62% | 13% | 18% | 0% | 19% |
| Conventional, waiver | 12% | 70% | 51% | 76% | 55% |
| Low-RVP | 21% | 15% | 15% | 23% | 16% |
| Clear (no Eoh) | 1% | 1% | 1% | 1% | 1% |
| Export | 3% | 1% | 15% | 0% | 10% |

Note: Low-RVP includes all non-waivered and low-RVP E10 gasoline.

- As noted in Section 1, additional RVP control through debutanization and depentanization leads to a loss of gasoline yield and octane. The models represent each regional refining sector replacing all the gasoline volume and octane lost in RVP control. The models represent the various options for volume and octane replacement discussed in Section 1. These include increasing crude runs, changing various refining operations (e.g., increasing reformer throughput and/or severity, increasing FCC unit conversion, and investing in additional refining process capacity).

Butane and pentane volumes rejected by the refining sector for RVP control in the summer season are assumed to be sold at regional prices estimated for the summer, based on average prices for butane at Mont Belvieu.

Regional energy prices – crude oil acquisition cost, natural gas prices, and power prices – in 2019 are estimated from EIA data.

- Other gasoline property standards represented in the Study and Sensitivity Cases are the same as in the Baseline Case (noted above).

Appendix A provides additional detail on and discussion of several aspects of the modeling methodology.

3. RESULTS OF THE ANALYSIS

3.1 Summary of Primary Results

Tables 3.1 and 3.2 show the estimated capital investment, annual refining cost, per-gallon refining cost, and energy density-related savings for the regional Study Cases and the Sensitivity Cases, respectively.

Table 3.1 Summary of Primary Results of the Study Case, by Region

| | Region | | | | Total |
|---|--------|--------|--------|--------|-------|
| | PADD 1 | PADD 2 | PADD 3 | PADD 4 | |
| Composite Crude Oil Cost (\$/b) | 66 | 57 | 62 | 54 | 61 |
| Finished Gasoline Volume ¹ (K b/d) | 66 | 1,546 | 2,351 | 270 | 4,233 |
| Capital Investment (\$MM) | 17 | 147 | 88 | 30 | 282 |
| Debutanization & Depentanization | 0 | 91 | 70 | 27 | 188 |
| All Other | 17 | 56 | 18 | 2 | 94 |
| Summer Refining Cost (\$MM) | 18 | 258 | 374 | 44 | 694 |
| Refining Operations | 14 | 214 | 347 | 35 | 610 |
| Capital Charge & Fixed Costs | 5 | 44 | 27 | 9 | 84 |
| Per-Gallon Refining Costs ² (¢/gal) | 3.6 | 2.2 | 2.1 | 2.1 | 2.1 |
| Refining Operations | 2.7 | 1.8 | 1.9 | 1.7 | 1.9 |
| Capital Charge & Fixed Costs | 0.9 | 0.4 | 0.1 | 0.4 | 0.3 |
| Energy Density-Related Savings ² (¢/gal) | 0.8 | 0.7 | 0.7 | 0.5 | 0.7 |

1 Summer E10 CG qualifying for the ethanol RVP waiver.

2 Per gallon of Summer E10 CG qualifying for the RVP waiver.

Table 3.2 Summary of Primary Results of the Sensitivity Case, by Region

| | Region | | | | Total |
|---|--------|--------|--------|--------|-------|
| | PADD 1 | PADD 2 | PADD 3 | PADD 4 | |
| Composite Crude Oil Cost (\$/b) | 107 | 94 | 101 | 89 | 100 |
| Finished Gasoline Volume ¹ (K b/d) | 66 | 1,546 | 2,351 | 270 | 4,233 |
| Capital Investment (\$MM) | 32 | 165 | 121 | 33 | 351 |
| Debutanization & Depentanization | 4 | 91 | 109 | 28 | 231 |
| All Other | 28 | 75 | 13 | 5 | 120 |
| Summer Refining Cost (\$MM) | 21 | 309 | 443 | 47 | 820 |
| Refining Operations | 12 | 261 | 406 | 36 | 714 |
| Capital Charge & Fixed Costs | 9 | 50 | 39 | 11 | 109 |
| Per-Gallon Refining Costs ² (¢/gal) | 4.2 | 2.6 | 2.5 | 2.3 | 2.5 |
| Refining Operations | 2.4 | 2.2 | 2.2 | 1.7 | 2.2 |
| Capital Charge & Fixed Costs | 1.8 | 0.4 | 0.2 | 0.5 | 0.3 |
| Energy Density-Related Savings ² (¢/gal) | 0.3 | 1.0 | 1.0 | 0.9 | 1.0 |

1 Summer E10 CG qualifying for the ethanol RVP waiver.

2 Per gallon of Summer E10 CG qualifying for the RVP waiver.

In these tables,

- **Capital Investments** (*CapEx*) reflect expansion of existing process units (that is, no grassroots investments are indicated in the solutions returned by the regional models).
- **Refining Operations** costs include catalysts and chemicals, changes in refinery inputs, additional energy use, and additional consumption (if any) of purchased hydrogen.
- **Per-Gallon Refining Cost** is the Summer Refining Cost allocated over the volume of affected E10 CG in the summer.
- **Energy Density-Related Savings** is the value of the small increase in energy density (BTU/gal) of the gasoline pool and hence vehicle fuel economy resulting from an 8 RVP standard for summer CBOB (allocated to the affected E10 CG).

The indicated Capital Investment for expansion of debutanization and depentanization are to achieve the specified RVP control. The Capital Investment for all other processes reflect expansion of minor processes needed to support debutanization or to maintain certain gasoline standards, such as benzene standards. The regional refinery models did not add new process capacity for octane replacement.

The estimated investment and annual refining costs of the 1 psi RVP reduction in the Study Case (\$61/b average crude oil price) are about **\$300 million** and **\$700 million/year**, respectively. The estimated average incremental cost of achieving the 1 psi RVP reduction standard is **2.1¢/gal** allocated across the affected summer E10 CG pool, with a high of **3.6¢/gal** in PADD 1 (where CBOB volume is low) and a low of **2.1¢/gal** in PADDs 3 and 4.⁶

The estimated investments and annual refining costs of meeting the 1 psi RVP reduction in the Sensitivity Case (\$100/b average crude oil price) are about **\$350 million** and **\$800 million/year**, respectively. The estimated incremental cost of achieving the 1 psi RVP reduction is **2.5¢/gal** allocated across the affected summer E10 CG pool, with a high of **4.2¢/gal** in PADD 1 (where CBOB volume is low) and a low of **2.3¢/gal** in PADD 4.

The line-item **Energy Density-Related Savings** in Table 3.1 (**0.7¢/gal**) and Table 3.2 (**1.0¢/gal**) denotes the estimated value of the small improvement in the energy density of the gasoline pool of producing summer CBOB meeting an 8 RVP standard, allocated over the affected E10 CG pool.

Appendix B presents additional, more detailed results of the analysis, in tabular form.

⁶ PADD 1 refineries produce a higher share of low-RVP gasoline and RFG than the other PADDs. We estimate that conventional gasoline (CG) constitutes only $\approx 12\%$ of gasoline production in PADD 1. According to our modeling results, this results in PADD 1 having much lower concentrations of C4s in the conventional gasoline pool than do other PADDs. This, in turn, increases the difficulty of RVP control in PADD 1 and requires depentanization to reduce the RVP of the relatively small share of E10 CG produced by PADD 1 refineries.

3.2 Discussion of Results

Comparison of the results of the Study Case (\$61/b average crude oil price) and the Sensitivity Case (\$100/b average crude oil price) indicates that the cost of the proposed 1 psi reduction in the RVP of summer CBOB is relatively insensitive to changes in the average crude oil price – even the substantial change embodied in the Sensitivity Case.

The Study and Sensitivity Cases call for similar changes in refining operations. The Sensitivity Case reflects the higher costs associated with the purchase of additional crude oil and slightly larger losses from the sales of butanes.

The expansion of process capacity in the solutions returned by the regional refinery models to meet the 1 psi reduction in CBOB RVP involves “minor” or “secondary” process units for which EIA does not report process capacities. The regional refinery models were set up so that “existing” capacity for such processes (1) reflected capacity from the 2016 Calibration cases from the recent study for EPA, and (2) incorporated minor capacity additions (if any) based on the calibration of those models to 2019. In the latter case, the refinery models are “tight” on those processes (just enough capacity). It may well be that refineries have sufficient capacity in these minor processes to increase RVP control without needing to expand capacity. If this were the case, Capital Investment could be significantly less than estimated here, and Per-Gallon Refining Cost would be closer to that in the sub-line-item labeled Refining Operations. In any case, the capital charges associated with our estimates of RVP control are low – about 0.3¢/gal.

The estimated **Energy Density-Related Savings** is a significant partial offset to the estimated refining cost of reducing the RVP of summer CBOB by 1 psi. These savings occur because removing C4 and C5 volumes from the gasoline pool to meet the more stringent RVP standard and replacing those volumes with heavier hydrocarbon blendstocks results in a small increase in the energy density of the gasoline pool, which in practice would bring about a corresponding small increase in average vehicle fuel economy. Consumers could purchase slightly less gasoline to drive the same number of miles. Hence, an increase in the gasoline pool’s average energy density would mean a decrease in total U.S. gasoline consumption (at constant vehicle miles traveled).

This decrease in gasoline consumption and consumer expenditures would accrue to consumers and would reduce the *national* cost (not the *refining* cost) of the 1 psi reduction in the RVP of summer CBOB. This cost savings would not accrue to refiners but would partially offset the refining cost of meeting the 8 RVP standard.

APPENDIX A: ADDITIONAL INFORMATION ON METHODOLOGY

A.1 RVP Representation

The regional models represent production of finished E10 gasolines, comprising base blends (CBOBs, Low-RVP BOBs, and RBOBs) produced at the refinery along with ethanol blended downstream of the refinery. The RVP limits for all gasolines (conventional and low-RVP) that qualify for the 1 psi ethanol RVP waiver are set at the RVP standard for those gasolines *ex the ethanol waiver*, adjusted for a 0.3 psi safety margin.⁷ The RVP of ethanol blended in those gasolines is set equal to their RVP standard (ex the ethanol waiver). The RVP limits for all gasolines not qualifying for the ethanol waiver – mostly RFG, but also some low-RVP and conventional gasoline – are set at the RVP standard for those gasolines, but, importantly, the RVP of ethanol blended in those gasolines is set so that it reflects its uplift on RVP. For the latter gasolines this forces the corresponding BOBs to have RVPs about 1.2 to 1.3 psi lower than the RVP standard for the finished gasoline.

The result is that the CBOB for E10 CG qualifying for the ethanol waiver has an RVP of 8.7 psi, whereas the “implicitly produced” RBOB for E10 RFG has an RVP of about 5.6 psi.

In the regional models’ representation of gasoline blending, blend RVP is computed using the RVP blending index (VPBI) method widely used in the refining industry.

The RVP blending index for each blend component is given by

$$\text{VPBI}_i = \text{RVP}_i^{1.2},$$

where the subscript *i* denotes the *i*th hydrocarbon blendstock. The computed RVP of the CBOB is then computed as

$$\text{RVP}_{\text{BOB}} = \Sigma i(\text{VPBI}_i)^{-1.2}$$

for each BOB represented in the regional models.

A.2 Representation of Capital Costs for RVP Control

As discussed earlier, refiners would meet a more stringent RVP standard through refinery-specific combinations of:

- Adding new, “grassroots” process units
- Expanding or revamping existing process units

⁷ To reflect (1) a safety margin in blending (to allow for measurement tolerances and pipeline receipt specifications) and (2) ethanol’s estimated effect on blend RVP (which is > 1 psi in summer E10 and increases slightly with decreasing base blend RVP).

- Changing operations in existing process units (e.g., increasing reformer throughput and severity, increasing crude oil throughput to support reforming and other processes, etc.)

The regional refining models represent one of the investment routes for each process represented in the models. We assumed that capital investment (*CapEx*)⁸ per unit of capacity added by expansions and revamps is 50% of the capital investment per unit of capacity (ISBL+OSBL) for a grassroots unit.⁹ All capacity additions in this study were based on these “expansion CapEx” factors.

Each process investment alternative is represented in terms of an estimated process-specific expansion capital cost (ISBL+OSBL) per b/d of throughput capacity added. These unit estimates represent the investments required for capacity increments corresponding to representative size units in U.S. refineries.

All capital costs are expressed in \$2019.

The unit CapEx factors available in the literature apply to a U.S. Gulf Coast location (i.e., PADD 3). These Gulf Coast factors are multiplied by regional escalation factors shown in below. to reflect the higher costs of refinery construction in the other PADDs.

- PADD 1: 1.5
- PADD 2: 1.3
- PADD 3: 1.0
- PADD 4: 1.4

In addition, for PADD 4, we increased the CapEx factors by 50% to reflect the adverse scale economies due to the small average size of the PADD 4 refineries.

For estimating the per-gallon annual capital charges associated with the CapEx for refining capacity, we used the following assumptions:

- Rate of return: 10% after tax¹⁰
- Operating life: 15 years
- Depreciation schedule: 10 year double declining balance
- Construction period: 3 years
- Tax rate: 40% (federal and state)

⁸ *CapEx* denotes capital investment.

⁹ *ISBL* and *OSBL* denote investments made Inside Battery Limits (i.e., for the process itself) and Outside Battery Limits (i.e., for off-site investments, such as utilities, tankage, etc.).

¹⁰ This rate of return typifies what refiners use when evaluating conventional refinery investment opportunities. EPA uses lower rates of return (e.g., 7% before tax) when estimating the “social” (national) costs of regulations.

An alternative set of assumptions regarding required rates of return – say 7% pre-tax – and a lower combined tax rate reflecting current federal corporate tax rates – say 26% – would reduce computed capital charges by about 30%.

APPENDIX B: DETAILED RESULTS OF THE REFINERY MODELING

Appendix B provides more detailed results from the refinery modeling for the Study and Sensitivity cases, in the form of six tables.

In the column headings of these tables, the words *Base* and *Study* denote the Reference and the 1 psi RVP Reduction cases, respectively. Further, in the body of these tables, the word *Primary* denotes the cases with 2019 crude oil acquisition costs.

Table B-1 shows selected refinery modeling results that highlight the most important changes in refining operations associated with reducing the RVP of CG BOBs: crude oil throughput increases; butane sales increase (with the exception of PADD 1, in which butane already is at low levels in E10 CG); debutanization, along with supporting process capacity, is added to remove butanes and maintain compliance with gasoline property standards; and reformer severity increases.

Table B-1: Selected Refinery Modeling Results for the Primary and Sensitivity Cases, by PADD

| Measure | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | Total | |
|------------------------------|--------|-------|--------|-------|--------|-------|--------|-------|--------|--------|
| | Base | Study | Base | Study | Base | Study | Base | Study | Base | Study |
| Primary | | | | | | | | | | |
| Crude Oil Use (K b/d) | 939 | 941 | 3,903 | 3,936 | 8,989 | 9,036 | 654 | 660 | 14,486 | 14,572 |
| Butane Sales (K b/d) | 13 | 13 | 71 | 96 | 75 | 114 | 3 | 7 | 161 | 230 |
| New Capacity (K b/cd) | | | | | | | | | | |
| Debutanization* | | | | 31 | | 31 | | 6 | | 68 |
| Depentanization | | | | | | | | 2 | | 2 |
| FCC Naphtha Desulfurization | | 13 | | | | 4 | | | | 18 |
| Benzene Saturation | | 1 | | 11 | | 3 | | | | 15 |
| Reformer Operations | | | | | | | | | | |
| Charge Rate (K b/d) | 142 | 139 | 690 | 694 | 1,603 | 1,611 | 100 | 103 | 2,535 | 2,546 |
| Severity (RON) | 96.5 | 98.0 | 94.0 | 95.5 | 95.7 | 96.0 | 93.3 | 94.1 | 95.2 | 95.9 |
| Sensitivity | | | | | | | | | | |
| Crude Oil Use (K b/d) | 940 | 941 | 3,901 | 3,933 | 8,989 | 9,035 | 654 | 660 | 14,484 | 14,570 |
| Butane Sales (K b/d) | 13 | 13 | 75 | 99 | 81 | 119 | 3 | 8 | 172 | 239 |
| New Capacity (K b/cd) | | | | | | | | | | |
| Debutanization* | | 1 | | 31 | | 48 | | 6 | | 86 |
| Depentanization | | 4 | | | | | | | | 4 |
| Naphtha Desulfurization | | | | | | | | 2 | | 2 |
| Light Naphtha Splitting | | 15 | | | | 4 | | | | 19 |
| Benzene Saturation | | 3 | | 13 | | 2 | | 1 | | 19 |
| Reformer Operations | | | | | | | | | | |
| Charge Rate (K b/d) | 146 | 142 | 711 | 704 | 1,620 | 1,614 | 101 | 105 | 2,577 | 2,565 |
| Severity (RON) | 96.8 | 97.1 | 93.4 | 95.1 | 95.7 | 96.0 | 93.9 | 94.2 | 95.0 | 95.7 |

Tables B-2a and B-2b show estimated use of existing process capacity, additions of new process capacity, refining operations and fuel use for the Primary and Sensitivity cases, respectively.

Table B-2a: Use of Existing Process Capacity, New Process Capacity, Refining Operations, and Fuel Use for the Primary Case, by PADD (K b/d, except as noted)

| Type of Process | Process | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | Total | |
|----------------------------------|----------------------------------|--------|-------|--------|--------|--------|--------|--------|-------|--------|--------|
| | | Base | Study | Base | Study | Base | Study | Base | Study | Base | Study |
| USE OF IN-PLACE CAPACITY | | | | | | | | | | | |
| Crude Distillation | Atmospheric | 939 | 941 | 3,903 | 3,936 | 8,989 | 9,036 | 654 | 660 | 14,486 | 14,572 |
| Conversion | Fluid Cat Cracker | 317 | 312 | 1,124 | 1,124 | 2,466 | 2,510 | 174 | 176 | 4,082 | 4,122 |
| | Hydrocracking | 36 | 36 | 342 | 342 | 1,076 | 1,076 | 26 | 26 | 1,480 | 1,480 |
| | Heavy Oil Hydrocracking | | | | | 110 | 110 | | | 110 | 110 |
| | Coking | 43 | 43 | 485 | 491 | 1,181 | 1,187 | 71 | 72 | 1,781 | 1,793 |
| Upgrading | Alkylation* | 70 | 70 | 239 | 239 | 553 | 553 | 41 | 41 | 902 | 902 |
| | Catalytic Polymerization* | 6 | 6 | 4 | 4 | 3 | | 5 | 5 | 18 | 15 |
| | Dimersol* | | | 1 | 1 | 10 | 10 | | | 11 | 11 |
| | Pen/Hex Isomerization | 6 | 6 | 112 | 112 | 174 | 174 | 5 | 5 | 298 | 298 |
| | Reforming | 137 | 137 | 652 | 665 | 1,543 | 1,555 | 97 | 101 | 2,429 | 2,458 |
| Hydrotreating | Naphtha Desulfurization | 247 | 252 | 1,053 | 1,064 | 2,303 | 2,315 | 172 | 174 | 3,775 | 3,805 |
| | FCC Naphtha Desulfurization | 172 | 169 | 630 | 630 | 1,285 | 1,315 | 98 | 98 | 2,185 | 2,213 |
| | Benzene Saturation | 16 | 16 | 28 | 28 | | | 9 | 9 | 53 | 53 |
| | Distillate Desulfurization | 285 | 286 | 1,157 | 1,179 | 2,752 | 2,753 | 227 | 225 | 4,421 | 4,443 |
| | FCC Feed Desulfurization (Conv) | 22 | 22 | 574 | 556 | 1,184 | 1,204 | 89 | 89 | 1,870 | 1,871 |
| Hydrogen (MM scf/d) | Hydrogen Production | 65 | 63 | 626 | 626 | 741 | 741 | 125 | 132 | 1,557 | 1,562 |
| | Hydrogen Recovery | 44 | 44 | 223 | 223 | 592 | 592 | 82 | 82 | 941 | 941 |
| Fractionation | Debutanization | 79 | 79 | 282 | 282 | 557 | 572 | 38 | 38 | 956 | 971 |
| | Lt. Naphtha Spl. (Benz. Prec.) | 53 | 53 | 214 | 190 | 763 | 763 | 52 | 52 | 1,081 | 1,057 |
| | Heavy FCC/Lt Cycle Oil Splitting | | | | | | | | | | |
| Other | Aromatics Plant* | 2 | 2 | 98 | 77 | 192 | 192 | | | 292 | 271 |
| | Benzene Extraction* | | | | | 12 | 12 | | | 12 | 12 |
| | Butane Isomerization | 12 | 12 | 11 | 11 | 71 | 71 | 2 | 2 | 96 | 96 |
| | Lubes & Waxes* | 13 | 13 | 8 | 8 | 139 | 139 | | | 160 | 160 |
| | Solvent Deasphalting | 13 | 13 | 17 | 17 | 196 | 196 | 5 | 5 | 231 | 231 |
| | Sulfur Recovery* (K std tons/d) | 1 | 1 | 6 | 6 | 10 | 10 | 1 | 1 | 17 | 17 |
| | Steam Generation (K lb/hr) | 3,038 | 3,060 | 11,434 | 11,581 | 33,693 | 33,825 | 1,897 | 1,937 | 50,062 | 50,403 |
| NEW CAPACITY (K b/d) | | | | | | | | | | | |
| Fractionation | Debutanization* | | | | 31 | | 31 | | 6 | | 68 |
| | Depentanization | | | | | | | | | | |
| | Light Naphtha Splitting | | 13 | | | | 4 | | | | 18 |
| Hydrotreating | FCC Naphtha Desulfurization | | | | | | | | 2 | | 2 |
| | Benzene Saturation | | 1 | | 11 | | 3 | | | | 15 |
| OPERATIONS & FUEL USE | | | | | | | | | | | |
| Fluid Cat Cracker | Charge Rate | 353 | 348 | 1,194 | 1,193 | 2,532 | 2,574 | 195 | 198 | 4,274 | 4,312 |
| | Conversion (Vol %) | 67 | 67 | 69 | 69 | 71 | 71 | 67 | 67 | 70 | 70 |
| | Olefin Max Cat. (%) | 37 | 39 | 6 | 5 | 54 | 50 | 23 | 24 | 38 | 36 |
| | European Yield Profile | | | | | | | | | | |
| Reformer | Charge Rate | 142 | 139 | 690 | 694 | 1,603 | 1,611 | 100 | 103 | 1159 | 1170 |
| | Severity (RON) | 96 | 98 | 94 | 95 | 96 | 96 | 93 | 94 | 95 | 96 |
| Fuel Use | Natural Gas (K foeb/d) | 24 | 24 | 85 | 84 | 199 | 199 | 19 | 20 | 327 | 325 |
| | Still Gas (K foeb/d) | 27 | 27 | 141 | 144 | 373 | 376 | 16 | 17 | 556 | 564 |
| | Catalyst Coke (K b/d) | 18 | 17 | 58 | 59 | 123 | 126 | 9 | 9 | 208 | 210 |

* In terms of product output.

Table B-2b: Use of Existing Process Capacity, New Process Capacity, Refining Operations, and Fuel Use for the Sensitivity Case, by PADD (K b/d, except as noted)

| Type of Process | Process | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | Total | |
|----------------------------------|----------------------------------|--------|-------|--------|--------|--------|--------|--------|-------|--------|--------|
| | | Base | Study | Base | Study | Base | Study | Base | Study | Base | Study |
| USE OF IN-PLACE CAPACITY | | | | | | | | | | | |
| Crude Distillation | Atmospheric | 940 | 941 | 3,901 | 3,933 | 8,989 | 9,035 | 654 | 660 | 14,484 | 14,570 |
| Conversion | Fluid Cat Cracker | 309 | 310 | 1,124 | 1,124 | 2,436 | 2,502 | 174 | 175 | 4,042 | 4,112 |
| | Hydrocracking | 36 | 36 | 342 | 342 | 1,076 | 1,076 | 26 | 26 | 1,480 | 1,480 |
| | Heavy Oil Hydrocracking | | | | | 110 | 110 | | | 110 | 110 |
| | Coking | 43 | 43 | 475 | 480 | 1,185 | 1,192 | 71 | 72 | 1,774 | 1,787 |
| Upgrading | Alkylation* | 70 | 70 | 239 | 239 | 553 | 553 | 41 | 41 | 902 | 902 |
| | Catalytic Polymerization* | 2 | 6 | | 4 | | | 2 | 2 | 4 | 12 |
| | Dimersol* | | | 1 | 1 | 15 | 15 | | | 16 | 16 |
| | Pen/Hex Isomerization | 6 | 6 | 112 | 112 | 174 | 174 | 5 | 5 | 298 | 298 |
| | Reforming | 142 | 139 | 667 | 673 | 1,558 | 1,558 | 99 | 103 | 2,466 | 2,473 |
| Hydrotreating | Naphtha Desulfurization | 249 | 249 | 1,055 | 1,065 | 2,312 | 2,321 | 172 | 174 | 3,788 | 3,810 |
| | FCC Naphtha Desulfurization | 171 | 167 | 617 | 613 | 1,261 | 1,304 | 101 | 101 | 2,149 | 2,185 |
| | Benzene Saturation | 17 | 17 | 31 | 31 | | | 9 | 9 | 58 | 58 |
| | Distillate Desulfurization | 285 | 285 | 1,178 | 1,201 | 2,760 | 2,772 | 231 | 229 | 4,454 | 4,487 |
| | FCC Feed Desulfurization (Conv) | 22 | 22 | 633 | 633 | 1,230 | 1,214 | 89 | 89 | 1,974 | 1,958 |
| | FCC Feed Desulfurization (Deep) | | | | | | | | | | |
| Hydrogen (MM scf/d) | Hydrogen Production | 84 | 84 | 626 | 626 | 741 | 741 | 135 | 138 | 1,586 | 1,589 |
| | Hydrogen Recovery | 44 | 44 | 223 | 223 | 592 | 592 | 82 | 82 | 941 | 941 |
| Fractionation | Debutanization | 79 | 79 | 283 | 283 | 572 | 572 | 38 | 38 | 971 | 972 |
| | Lt. Naphtha Spl. (Benz. Prec.) | 53 | 53 | 203 | 180 | 764 | 764 | 52 | 52 | 1,071 | 1,047 |
| | Heavy FCC/Lt Cycle Oil Splitting | | | | | | | 2 | | 2 | |
| Other | Aromatics Plant* | 2 | 2 | 100 | 77 | 192 | 192 | | | 295 | 271 |
| | Benzene Extraction* | | | | | 12 | 12 | | | 12 | 12 |
| | Butane Isomerization | 12 | 12 | 11 | 11 | 71 | 71 | 2 | 2 | 96 | 96 |
| | Lubes & Waxes* | 13 | 13 | 8 | 8 | 139 | 139 | | | 160 | 160 |
| | Solvent Deasphalting | 13 | 13 | 17 | 17 | 196 | 196 | 5 | 5 | 231 | 231 |
| | Sulfur Recovery* (K std tons/d) | 1 | 1 | 6 | 6 | 10 | 10 | 1 | 1 | 17 | 17 |
| | Steam Generation (K lb/hr) | 3,017 | 3,099 | 11,826 | 12,088 | 33,864 | 33,833 | 1,889 | 1,915 | 50,597 | 50,935 |
| NEW CAPACITY (K b/sd) | | | | | | | | | | | |
| Fractionation | Debutanization* | | 1 | | 31 | | 48 | | 6 | | 86 |
| | Depentanization | | 4 | | | | | | | | 4 |
| | Light Naphtha Splitting | | 15 | | | | 4 | | | | 19 |
| Hydrotreating | Naphtha Desulfurization | | | | 13 | | | | 2 | | 2 |
| | Benzene Saturation | | 3 | | | | 2 | | 1 | | 19 |
| OPERATIONS & FUEL USE | | | | | | | | | | | |
| Fluid Cat Cracker | Charge Rate | 342 | 343 | 1,114 | 1,115 | 2,496 | 2,575 | 196 | 198 | 4,148 | 4,230 |
| | Conversion (Vol %) | 67 | 67 | 73 | 73 | 71 | 71 | 66 | 66 | 71 | 71 |
| | Olefin Max Cat. (%) | 23 | 38 | 2 | 6 | 51 | 46 | 6 | 6 | 33 | 33 |
| | European Yield Profile | | | 31 | 31 | 20 | 20 | | | 51 | 51 |
| Reformer | Charge Rate | 146 | 142 | 711 | 704 | 1,620 | 1,614 | 101 | 105 | 1182 | 1184 |
| | Severity (RON) | 97 | 97 | 93 | 95 | 96 | 96 | 94 | 94 | 95 | 96 |
| Fuel Use | Natural Gas (K foeb/d) | 24 | 24 | 90 | 88 | 202 | 199 | 20 | 20 | 335 | 332 |
| | Still Gas (K foeb/d) | 27 | 27 | 139 | 143 | 373 | 377 | 16 | 16 | 555 | 563 |
| | Catalyst Coke (K b/d) | 17 | 17 | 55 | 55 | 121 | 125 | 9 | 9 | 202 | 206 |

* In terms of product output.

Tables B-3a and B-3b show estimated refining sector input and output volumes for the Primary and Sensitivity cases, respectively.

Table B-3a: Refinery Inputs and Outputs for the Primary Case, by PADD (K b/d, except as noted)

| Inputs/ Outputs | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | Total | |
|-------------------------------------|--------|-------|--------|-------|--------|-------|--------|-------|--------|--------|
| | Base | Study | Base | Study | Base | Study | Base | Study | Base | Study |
| INPUTS | | | | | | | | | | |
| Crude Oil | 939 | 941 | 3,903 | 3,936 | 8,989 | 9,036 | 654 | 660 | 14,486 | 14,572 |
| Renewable Fuel Inputs | 57 | 57 | 225 | 225 | 393 | 393 | 38 | 38 | 713 | 713 |
| Ethanol | 56 | 56 | 219 | 219 | 392 | 392 | 36 | 36 | 703 | 703 |
| Biodiesel/Renewable Diesel | 1 | 1 | 6 | 6 | 2 | 2 | 2 | 2 | 9 | 9 |
| Other Inputs | 70 | 71 | 81 | 79 | 704 | 701 | 22 | 21 | 877 | 871 |
| Isobutane | 11 | 12 | 49 | 47 | 142 | 139 | 7 | 6 | 209 | 203 |
| Butane | | | | | | | | | | |
| Butylene | 1 | 1 | | | 9 | 9 | | | 10 | 10 |
| Natural Gasoline | 2 | 2 | 25 | 25 | 96 | 96 | 5 | 5 | 128 | 128 |
| Straight Run Naphtha | 21 | 21 | 4 | 4 | | | | | 25 | 25 |
| Kerosene | | | 3 | 3 | 4 | 4 | | | 7 | 7 |
| Heavy Gas Oil | 29 | 29 | | | 341 | 341 | 10 | 10 | 380 | 380 |
| Resid | 6 | 6 | | | 112 | 112 | | | 118 | 118 |
| Purchased Energy & H2 | | | | | | | | | | |
| Electricity (MM Kwh/d) | 6 | 6 | 29 | 29 | 70 | 71 | 4 | 4 | 109 | 110 |
| Natural Gas (K foeb/d) | 26 | 26 | 109 | 107 | 228 | 227 | 24 | 25 | 387 | 385 |
| Hydrogen (K foeb/d) | | | 33 | 34 | 121 | 120 | | | 153 | 154 |
| OUTPUTS | | | | | | | | | | |
| Refined Products | 1,049 | 1,049 | 4,095 | 4,122 | 9,906 | 9,946 | 693 | 698 | 15,742 | 15,815 |
| Aromatics | 1 | 1 | 60 | 60 | 179 | 179 | | | 240 | 240 |
| Ethane/Ethylene | | | | | 5 | 5 | | | 5 | 5 |
| Propane | 14 | 14 | 59 | 61 | 157 | 158 | 9 | 9 | 239 | 243 |
| Propylene | 14 | 14 | 41 | 41 | 225 | 225 | | | 280 | 280 |
| Butanes/Butylenes | 13 | 13 | 71 | 96 | 75 | 114 | 3 | 7 | 161 | 230 |
| Pentanes | | | | | | | | | | |
| Y-Grade | | | | | 171 | 171 | | | 171 | 171 |
| Condensate | | | | | | | | | | |
| Aviation Gas | | | 1 | 1 | 10 | 10 | | | 11 | 11 |
| Special Naphthas | 1 | 1 | | | 30 | 30 | | | 31 | 31 |
| Gasoline: | 532 | 532 | 2,198 | 2,198 | 4,642 | 4,642 | 356 | 356 | 7,728 | 7,728 |
| E10 RFG -- Premium | 48 | 48 | 30 | 30 | 121 | 121 | | | 199 | 199 |
| Regular | 284 | 284 | 248 | 248 | 709 | 709 | | | 1,241 | 1,241 |
| E10 Conventional -- Premium | 6 | 6 | 127 | 127 | 295 | 295 | 46 | 46 | 474 | 474 |
| Reg | 60 | 60 | 1,419 | 1,419 | 2,056 | 2,056 | 224 | 224 | 3,759 | 3,759 |
| E10 Low-RVP ² -- Premium | 10 | 10 | 27 | 27 | 69 | 69 | 15 | 15 | 121 | 121 |
| Regular | 102 | 102 | 313 | 313 | 644 | 644 | 68 | 68 | 1,127 | 1,127 |
| Clear Finished | 5 | 5 | 21 | 21 | 32 | 32 | 3 | 3 | 61 | 61 |
| Exported | 17 | 17 | 13 | 13 | 716 | 716 | | | 746 | 746 |
| E85 | 7 | 7 | 4 | 4 | 3 | 3 | 1 | 1 | 15 | 15 |
| Jet Fuel | 110 | 110 | 288 | 288 | 952 | 952 | 41 | 41 | 1,391 | 1,391 |
| Diesel Fuel | 278 | 278 | 1,136 | 1,136 | 2,957 | 2,957 | 220 | 220 | 4,591 | 4,591 |
| Ultra Low Sulfur Diesel | 271 | 271 | 1,136 | 1,136 | 2,672 | 2,672 | 219 | 219 | 4,298 | 4,298 |
| CARB Diesel | | | | | | | | | | |
| EPA Diesel | 3 | 3 | | | 103 | 103 | 1 | 1 | 107 | 107 |
| Off road diesel/HH Oil | 4 | 4 | | | 182 | 182 | | | 186 | 186 |
| Unf. Oil to PetroChem | | | 34 | 34 | 97 | 97 | 8 | 8 | 139 | 139 |
| Residual Oil | 36 | 36 | 52 | 52 | 183 | 183 | 14 | 14 | 285 | 285 |
| Low Sulfur | 5 | 5 | 2 | 2 | 42 | 42 | 6 | 6 | 55 | 55 |
| Medium Sulfur & Marpol | 17 | 17 | 5 | 5 | 19 | 19 | 1 | 1 | 42 | 42 |
| High Sulfur | 14 | 14 | 45 | 45 | 122 | 122 | 7 | 7 | 188 | 188 |
| Asphalt | 37 | 37 | 147 | 147 | 84 | 84 | 42 | 42 | 310 | 310 |
| Lubes & Waxes | 13 | 13 | 8 | 8 | 139 | 139 | | | 160 | 160 |
| Other | | | | | | | | | | |
| Coke | 12 | 12 | 165 | 167 | 336 | 338 | 22 | 22 | 535 | 539 |
| Sulfur (Std tons/d) | 1 | 1 | 6 | 6 | 10 | 10 | 1 | 1 | 17 | 17 |

**Table B-3b: Refinery Inputs and Outputs for the Sensitivity Case, by PADD
(K b/d, except as noted)**

| Inputs/ Outputs | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | Total | |
|-------------------------------------|--------------|--------------|--------------|--------------|--------------|--------------|------------|------------|---------------|---------------|
| | Base | Study | Base | Study | Base | Study | Base | Study | Base | Study |
| INPUTS | | | | | | | | | | |
| Crude Oil | 940 | 941 | 3,901 | 3,933 | 8,989 | 9,035 | 654 | 660 | 14,484 | 14,570 |
| Renewable Fuel Inputs | 57 | 57 | 225 | 225 | 393 | 393 | 38 | 38 | 713 | 713 |
| Ethanol | 56 | 56 | 219 | 219 | 392 | 392 | 36 | 36 | 703 | 703 |
| Biodiesel/Renewable Diesel | 1 | 1 | 6 | 6 | 2 | 2 | 2 | 2 | 9 | 9 |
| Other Inputs | 69 | 70 | 81 | 79 | 699 | 697 | 21 | 20 | 869 | 866 |
| Isobutane | 10 | 11 | 49 | 47 | 137 | 135 | 6 | 5 | 201 | 198 |
| Butane | | | | | | | | | | |
| Butylene | 1 | 1 | | | 9 | 9 | | | 10 | 10 |
| Natural Gasoline | 2 | 2 | 25 | 25 | 96 | 96 | 5 | 5 | 128 | 128 |
| Straight Run Naphtha | 21 | 21 | 4 | 4 | | | | | 25 | 25 |
| Kerosene | | | 3 | 3 | 4 | 4 | | | 7 | 7 |
| Heavy Gas Oil | 29 | 29 | | | 341 | 341 | 10 | 10 | 380 | 380 |
| Resid | 6 | 6 | | | 112 | 112 | | | 118 | 118 |
| Purchased Energy & H2 | | | | | | | | | | |
| Electricity (MM Kwh/d) | 6 | 6 | 29 | 29 | 71 | 71 | 4 | 4 | 109 | 110 |
| Natural Gas (K foeb/d) | 27 | 28 | 114 | 112 | 230 | 228 | 25 | 25 | 396 | 393 |
| Hydrogen (K foeb/d) | | | 37 | 39 | 128 | 126 | | | 165 | 165 |
| OUTPUTS | | | | | | | | | | |
| Refined Products | 1,049 | 1,051 | 4,098 | 4,125 | 9,911 | 9,950 | 693 | 698 | 15,751 | 15,825 |
| Aromatics | 1 | 1 | 60 | 60 | 179 | 179 | | | 240 | 240 |
| Ethane/Ethylene | | | | | 5 | 5 | | | 5 | 5 |
| Propane | 14 | 14 | 59 | 61 | 156 | 157 | 9 | 9 | 238 | 242 |
| Propylene | 14 | 14 | 41 | 41 | 225 | 225 | | | 280 | 280 |
| Butanes/Butylenes | 13 | 13 | 75 | 99 | 81 | 119 | 3 | 8 | 172 | 239 |
| Pentanes | | 2 | | | | | | | | 2 |
| Y-Grade | | | | | 171 | 171 | | | 171 | 171 |
| Condensate | | | | | | | | | | |
| Aviation Gas | | | 1 | 1 | 10 | 10 | | | 11 | 11 |
| Special Naphthas | 1 | 1 | | | 30 | 30 | | | 31 | 31 |
| Gasoline: | 532 | 532 | 2,198 | 2,198 | 4,642 | 4,642 | 356 | 356 | 7,728 | 7,728 |
| E10 RFG -- Premium | 48 | 48 | 30 | 30 | 121 | 121 | | | 199 | 199 |
| Regular | 284 | 284 | 248 | 248 | 709 | 709 | | | 1,241 | 1,241 |
| E10 Conventional -- Premium | 6 | 6 | 127 | 127 | 295 | 295 | 46 | 46 | 474 | 474 |
| Reg | 60 | 60 | 1,419 | 1,419 | 2,056 | 2,056 | 224 | 224 | 3,759 | 3,759 |
| E10 Low-RVP ² -- Premium | 10 | 10 | 27 | 27 | 69 | 69 | 15 | 15 | 121 | 121 |
| Regular | 102 | 102 | 313 | 313 | 644 | 644 | 68 | 68 | 1,127 | 1,127 |
| Clear Finished | 5 | 5 | 21 | 21 | 32 | 32 | 3 | 3 | 61 | 61 |
| Exported | 17 | 17 | 13 | 13 | 716 | 716 | | | 746 | 746 |
| E85 | 7 | 7 | 4 | 4 | 3 | 3 | 1 | 1 | 15 | 15 |
| Jet Fuel | 110 | 110 | 288 | 288 | 952 | 952 | 41 | 41 | 1,391 | 1,391 |
| Diesel Fuel | 278 | 278 | 1,136 | 1,136 | 2,957 | 2,957 | 220 | 220 | 4,591 | 4,591 |
| Ultra Low Sulfur Diesel | 271 | 271 | 1,136 | 1,136 | 2,672 | 2,672 | 219 | 219 | 4,298 | 4,298 |
| CARB Diesel | | | | | | | | | | |
| EPA Diesel | 3 | 3 | | | 103 | 103 | 1 | 1 | 107 | 107 |
| Off road diesel/HH Oil | 4 | 4 | | | 182 | 182 | | | 186 | 186 |
| Unf. Oil to PetroChem | | | 34 | 34 | 97 | 97 | 8 | 8 | 139 | 139 |
| Residual Oil | 36 | 36 | 52 | 52 | 183 | 183 | 14 | 14 | 285 | 285 |
| Low Sulfur | 5 | 5 | 2 | 2 | 42 | 42 | 6 | 6 | 55 | 55 |
| Medium Sulfur & Marpol | 17 | 17 | 5 | 5 | 19 | 19 | 1 | 1 | 42 | 42 |
| High Sulfur | 14 | 14 | 45 | 45 | 122 | 122 | 7 | 7 | 188 | 188 |
| Asphalt | 37 | 37 | 147 | 147 | 84 | 84 | 42 | 42 | 310 | 310 |
| Lubes & Waxes | 13 | 13 | 8 | 8 | 139 | 139 | | | 160 | 160 |
| Other | | | | | | | | | | |
| Coke | 12 | 12 | 163 | 165 | 336 | 338 | 22 | 22 | 533 | 537 |
| Sulfur (Std tons/d) | 1 | 1 | 6 | 6 | 10 | 10 | 1 | 1 | 17 | 17 |

Table B-4 shows the estimated volume-weighted composition (by blendstock) of the finished E10 conventional gasoline pool for the Primary and Sensitivity cases. The compositions of the RFG, low-RVP, and export gasoline pools in the Study cases were *not* constrained to remain the same as in the Base cases. Thus, the composition of those finished gasoline pools, as returned by the refinery model, changed somewhat in response to required reductions in the RVP of CBOB.

Table B-4: Composition of Finished E10 CG for the Primary and Sensitivity Cases, by PADD

| Gasoline Blendstock | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | Total | |
|----------------------------|-----------|-----------|--------------|--------------|--------------|--------------|------------|------------|--------------|--------------|
| | Base | Study | Base | Study | Base | Study | Base | Study | Base | Study |
| Primary (K b/d) | 66 | 66 | 1,546 | 1,546 | 2,351 | 2,351 | 270 | 270 | 4,233 | 4,233 |
| C4s | 0.8% | 0.5% | 2.3% | 1.0% | 2.8% | 1.1% | 3.7% | 2.5% | 2.6% | 1.2% |
| Natural Gas Liquids | | 0.3% | 1.5% | 1.5% | 4.1% | 3.6% | 0.1% | 1.8% | 2.8% | 2.7% |
| C5s & Isomerate | 0.5% | | 7.1% | 6.6% | 3.9% | 5.6% | | 1.6% | 4.8% | 5.6% |
| Raffinate | 3.5% | 1.0% | 5.3% | 1.4% | 0.7% | 5.8% | | | 2.3% | 3.8% |
| Naphthas (C5-250°) | 21.5% | 25.8% | 9.3% | 14.9% | 8.8% | 10.6% | 15.3% | 18.9% | 9.6% | 12.9% |
| Hydrocrackate | 6.5% | 1.1% | 6.3% | 6.3% | 11.5% | 11.6% | 2.1% | 2.3% | 8.9% | 8.9% |
| Alkylate | 0.4% | 1.1% | 12.3% | 11.9% | 7.9% | 10.5% | 8.5% | 13.7% | 9.4% | 11.1% |
| Poly Gas | 4.1% | | 0.1% | | 0.1% | | | 1.0% | 0.2% | 0.1% |
| FCC Naphtha | 7.5% | 23.9% | 35.4% | 29.7% | 36.8% | 19.5% | 35.2% | 29.1% | 35.8% | 23.9% |
| Reformate & Aromatics | 45.2% | 36.4% | 10.3% | 16.6% | 13.5% | 21.8% | 25.2% | 19.1% | 13.6% | 20.0% |
| Ethanol | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% |
| Sensitivity (K b/d) | 66 | 66 | 1,546 | 1,546 | 2,351 | 2,351 | 270 | 270 | 4,233 | 4,233 |
| C4s | 0.5% | 0.5% | 2.3% | 1.0% | 2.4% | 1.0% | 3.6% | 2.0% | 2.4% | 1.1% |
| Natural Gas Liquids | | | 1.5% | 1.5% | 4.1% | 4.1% | 1.8% | 1.8% | 2.9% | 2.9% |
| C5s & Isomerate | 1.3% | 0.5% | 6.5% | 4.4% | 5.5% | 6.8% | 0.9% | 1.5% | 5.5% | 5.5% |
| Raffinate | 3.9% | 0.4% | 6.4% | 4.3% | 5.6% | 0.4% | | | 5.5% | 1.8% |
| Naphthas (C5-250°) | 18.2% | 16.4% | 9.4% | 12.8% | 8.4% | 11.1% | 17.9% | 14.3% | 9.5% | 12.0% |
| Hydrocrackate | 7.5% | 11.6% | 6.6% | 6.9% | 3.9% | 0.1% | 2.3% | 2.5% | 4.9% | 2.9% |
| Alkylate | 0.4% | 0.7% | 7.8% | 4.5% | 2.5% | 7.0% | 9.5% | 12.6% | 4.8% | 6.4% |
| Poly Gas | | 0.7% | 0.0% | | | | 0.3% | 0.5% | 0.0% | 0.0% |
| FCC Naphtha | 16.9% | 29.1% | 30.9% | 26.9% | 35.2% | 46.0% | 34.6% | 34.4% | 33.3% | 38.0% |
| Reformate & Aromatics | 41.3% | 30.0% | 18.6% | 27.6% | 22.5% | 13.6% | 19.1% | 20.6% | 21.2% | 19.4% |
| Ethanol | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% | 10.0% |

Note: The composition of the non-conventional gasoline pool was *not* fixed at the base case composition in the RVP cases. However, all octane and RVP constraints for the non-conventional gasoline pool had to be satisfied.

Table B-5 shows the estimated properties of the finished E10 conventional gasoline pool for the Primary and Sensitivity cases.

The RVP of the finished CG pool declines by about 0.9 psi, consistent with a 1 psi reduction in the RVP of CBOB (from 8.7 psi to 7.7 psi) and an RVP uplift from ethanol blending of about 1.2 psi.

Other properties of the finished CG pool (octane and benzene and sulfur content) were constrained to meet the same standards as in the Base cases. Likewise, certain properties (octane, RVP, and benzene and sulfur content) of the finished reformulated, low-RVP, and export gasoline pools were constrained to meet the same standards in the Study cases as in the Base cases.

Table B-5: Properties of Finished E10 CG for the Primary and Sensitivity Cases, by PADD

| Properties | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | Total | |
|---|-----------|-----------|--------------|--------------|--------------|--------------|------------|------------|--------------|--------------|
| | Base | Study | Base | Study | Base | Study | Base | Study | Base | Study |
| Primary (K b/d) | 66 | 66 | 1,546 | 1,546 | 2,351 | 2,351 | 270 | 270 | 4,233 | 4,233 |
| RVP (psi) | 9.8 | 8.9 | 9.8 | 8.9 | 9.8 | 8.9 | 9.8 | 8.9 | 9.8 | 8.9 |
| Fuel Ethanol (vol%) | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Aromatics (vol%) | 23.9 | 26.9 | 14.5 | 16.6 | 17.5 | 17.5 | 20.4 | 17.3 | 16.7 | 17.3 |
| Benzene (vol%) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| Olefins (vol%) | 5.9 | 5.6 | 7.8 | 6.6 | 8.5 | 4.3 | 7.5 | 7.1 | 8.1 | 5.4 |
| Sulfur (ppm) | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| E200 (vol% off) | 58.1 | 55.5 | 55.3 | 55.0 | 56.7 | 56.5 | 53.3 | 53.1 | 56.0 | 55.7 |
| E300 (vol% off) | 94.7 | 85.5 | 84.3 | 84.4 | 85.1 | 81.9 | 82.6 | 82.4 | 84.8 | 82.9 |
| Energy Density ¹ | 4.677 | 4.728 | 4.637 | 4.653 | 4.654 | 4.670 | 4.697 | 4.683 | 4.651 | 4.665 |
| Octane | | | | | | | | | | |
| (R+M)/2 | 88.0 | 88.0 | 87.9 | 87.9 | 88.1 | 88.1 | 87.6 | 87.6 | 88.0 | 88.0 |
| MON | 83.7 | 83.2 | 83.5 | 83.6 | 83.5 | 83.7 | 82.9 | 83.2 | 83.4 | 83.6 |
| RON | 92.3 | 92.7 | 92.3 | 92.2 | 92.7 | 92.4 | 92.4 | 92.1 | 92.5 | 92.3 |
| Sensitivity | 9.3 | 9.3 | 8.9 | 9.0 | 9.4 | 8.8 | 8.9 | 9.0 | 9.2 | 8.9 |
| Sensitivity (K b/d) | 66 | 66 | 1,546 | 1,546 | 2,351 | 2,351 | 270 | 270 | 4,233 | 4,233 |
| RVP (psi) | 9.8 | 8.9 | 9.8 | 8.9 | 9.8 | 8.9 | 9.8 | 8.9 | 9.8 | 8.9 |
| Fuel Ethanol (vol%) | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Aromatics (vol%) | 24.1 | 25.4 | 18.7 | 22.2 | 21.9 | 19.8 | 17.5 | 17.7 | 20.5 | 20.6 |
| Benzene (vol%) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| Olefins (vol%) | 4.5 | 7.5 | 7.1 | 6.1 | 8.0 | 10.0 | 7.7 | 7.7 | 7.6 | 8.4 |
| Sulfur (ppm) | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 |
| E200 (vol% off) | 58.3 | 55.1 | 55.7 | 52.9 | 53.9 | 53.6 | 52.9 | 53.6 | 54.6 | 53.4 |
| E300 (vol% off) | 94.4 | 80.5 | 82.7 | 81.6 | 81.0 | 81.5 | 84.1 | 84.6 | 82.1 | 81.7 |
| Energy Density ¹ | 4.679 | 4.707 | 4.673 | 4.712 | 4.719 | 4.704 | 4.677 | 4.679 | 4.699 | 4.705 |
| Octane | | | | | | | | | | |
| (R+M)/2 | 88.0 | 88.0 | 87.9 | 87.9 | 88.1 | 88.1 | 87.6 | 87.6 | 88.0 | 88.0 |
| MON | 83.6 | 83.0 | 83.3 | 83.1 | 83.0 | 83.0 | 83.1 | 83.1 | 83.1 | 83.1 |
| RON | 92.4 | 92.9 | 92.5 | 92.7 | 93.1 | 93.1 | 92.2 | 92.1 | 92.8 | 92.9 |
| Sensitivity | 9.3 | 9.3 | 9.0 | 9.1 | 9.1 | 9.2 | 8.9 | 9.0 | 9.1 | 9.1 |
| Energy Density of Entire Gasoline Pool¹ | | | | | | | | | | |
| Primary Cases | 4.729 | 4.731 | 4.683 | 4.696 | 4.724 | 4.733 | 4.685 | 4.697 | 4.711 | 4.720 |
| Sensitivity Cases | 4.729 | 4.730 | 4.686 | 4.698 | 4.723 | 4.731 | 4.685 | 4.698 | 4.711 | 4.720 |

¹ Lower heating value (MM btu/b).

Table B-6 shows the estimated crude oil acquisition costs and the prices for butane, natural gas, and power estimated for the summer of 2019 and used in the refinery modeling. Crude oil acquisition costs, natural gas prices (the lower of industrial or city gate prices), and power prices (retail prices to industrial users) were derived from data reported by EIA. Butane prices were estimated from monthly average spot prices at Mt. Belvieu from Bloomberg, as reported by EIA, with some PADD-level adjustments.

Composite prices for crude oil in the Sensitivity cases were based on an assumed U.S. average cost of composite crude oil of \$100/b, with PADD-level adjustments based on relative PADD-level crude oil costs over the past decade. Butane prices in the Sensitivity cases were adjusted upwards based on the relationship of butane prices to crude oil costs over the past decade. Natural gas and power prices in the Sensitivity cases were assumed to remain at those estimated for the summer of 2019.

Table B-6: Composite Cost of Crude Oil and Prices for Butane, Natural Gas, and Power Used in Refinery Modeling for the Primary and Sensitivity Cases, by PADD

| | PADD 1 | | PADD 2 | | PADD 3 | | PADD 4 | | U.S. Average |
|-----------------------|--------|-------|--------|-------|--------|-------|--------|-------|--------------|
| | Base | Study | Base | Study | Base | Study | Base | Study | |
| Primary | | | | | | | | | |
| Crude Oil (\$/b) | 65.8 | 65.8 | 56.7 | 56.7 | 62.0 | 62.0 | 54.4 | 54.4 | 61.0 |
| Butane (\$/b) | 27.6 | 27.6 | 23.0 | 23.0 | 23.6 | 23.6 | 23.0 | 23.0 | - |
| Natural Gas (\$/foeb) | 42.4 | 42.4 | 21.8 | 21.8 | 18.0 | 18.0 | 18.1 | 18.1 | 21.0 |
| Power (¢/kwh) | 7.9 | 7.9 | 6.6 | 6.6 | 5.4 | 5.4 | 6.2 | 6.2 | 6.0 |
| Sensitivity | | | | | | | | | |
| Crude Oil (\$/b) | 106.6 | 106.6 | 93.9 | 93.9 | 101.4 | 101.4 | 88.7 | 88.7 | 100.0 |
| Butane (\$/b) | 63.2 | 63.2 | 56.2 | 56.2 | 59.2 | 59.2 | 56.2 | 56.2 | - |
| Natural Gas (\$/foeb) | 42.4 | 42.4 | 21.8 | 21.8 | 18.0 | 18.0 | 18.1 | 18.1 | 21.0 |
| Power (¢/kwh) | 7.9 | 7.9 | 6.6 | 6.6 | 5.4 | 5.4 | 6.2 | 6.2 | 6.0 |